

MULTISTAGE ADAPTIVE PARALLEL INTERFERENCE CANCELLER

Technical Field

5 The present invention relates to a multistage adaptive partial parallel interference canceller which efficiently cancels multiple access interference (MAI) and interpath interference (IPI) in a direct sequence code division multiple access (DS-CDMA) mobile communication system.

10

Background Art

 The performance of the third generation CDMA systems for providing upto 2 Mbps data rate is always degraded by multiple access interference (MAI) and interpath interference (IPI). Also, although orthogonal codes are used, orthogonal characteristics of codes are corrupted on a time varying fading channel and a rake receiver produces more complicated interference for high data rate channels. 15
20 These also makes multi-user detection (MUD) design complicated.

 When a multi-rate system is implemented to provide multimedia services to each user, the design of MUD becomes more complicated and it results in the performance degradation of the low data rate channels because a channel having a low data rate experiences severe interference from a channels having a high data rate. 25

In order to overcome the problems, concepts of MUD have been proposed and research results have been presented. The research results include a maximum likelihood sequence (MLS) detector, a linear MUD, a neural network based MUD
5 and a nonlinear MUD.

However, the MLS detector has disadvantages such as exponentially increasing complexity and difficulty of a real-time implementation as the number of users is increased. The linear MUD has great performance at white
10 noise environment, but the performance of the system is degraded on a time varying fading channel. In order to overcome the problem on the time varying channel, the adaptive linear MUDs have been proposed. However, the efficiency of channel usage is degraded because training
15 sequences are required and the time varying characteristic of correlation coefficients among signature waveforms of high data rate channels is too fast to adjust and to estimate in real time.

There are MUDs based on neural network such as
20 Multilayer Cerptron (MLP) or Hopfield Neural Network (HNN). The MLP has disadvantages that the channel efficiency is degraded because training sequences are required and faster back propagation algorithm is necessary as the number of users increases and it results in an increase of the number
25 of neurons. Also, the HNN has a disadvantage that the number of local minimums increases and the global minimum may not be founded, as the number of users increases.

The nonlinear MUD such as Parallel Interference Canceller (PIC) is known to be a practical structure for overcoming the difficulty for estimating the fast time variant correlation coefficients among signature waveforms even though the circuit is complicate. Especially, the multistage parallel interference canceller (MPIC) 15 is recognized as a very efficient device for low data rate channels among MUDs.

Fig. 1 is a block diagram showing a conventional multistage parallel interference canceller (PIC) having hard limiters.

Referring to Fig. 1, $r(t)$ is a signal received by a rake receiver 10 and MAI and IPI are cancelled by a multistage PIC.

Fig. 2 is a block diagram showing an internal structure of the i^{th} interference canceller in Fig. 1. Herein, i denotes the i^{th} interference canceller, and j denotes the j^{th} channel.

Referring to Fig. 2, a hard limiter 20 of each channel performs hard decisions on a input signals and generates digital signals such as +1 or -1. The digital signal is re-spread by a Walsh code $W(t)$ and a scrambling code $S(t)$ and inputted to an the interference generator 22.

The interference generator 22 computes total interference signals $I_{ij}(t)$ including MAI as follows.

For $j=1$ to 4 and $i=1$ to N

$$z_{oij}(t) = (\bar{a}_{ij}(t)z_{ij}(t) + \bar{b}_{ij}(t-3T_c)z_{ij}(t-3T_c) + \bar{c}_{ij}(t-5T_c)z_{ij}(t-5T_c))$$

$$I_{ij}(t) = \sum_{l=1}^4 z_{oil}(t)$$

Eq. 1

5 The computed total interference signals $I_{ij}(t)$ are removed from the signal $r_i(t)$ inputted to the rake receiver 24 and a signal x_{ij} is outputted from the rake receiver 24. Herein, $a_{ij}(t)$, $b_{ij}(t)$ and $c_{ij}(t)$ are tap gains outputted from the channel estimator of the rake receiver 24. That is, $a_{i3}(t)$,
10 $b_{i3}(t)$ and $c_{i3}(t)$ are tap gains of the third user channel in the i^{th} interference canceller.

 The matched filter receives the signal $x_{i+1,j}$ outputted from the rake receiver 24, extracts signal components for each channel and outputs the extracted signal components to
15 an $i+1^{\text{th}}$ interference canceller. As mentioned above, interference signals are computed more precisely as the number of stages increases and interference cancelled and correctly detected signals for each channel can be obtained by the final parallel interference canceller (PIC).

20 A performance of the multistage PIC mainly depends on the initial decision of the limiter. If the hard decision at the initial stage is wrong, wrong interference signals are generated and the performance of the multistage PIC is abruptly degraded. That is to say, the error of the
25 initial stage is not removed and continuously affects interference cancellation. Finally, it results in overflow

of detected errors.

To overcome the problem mentioned above, a multistage partial PICs have been proposed. The multistage partial PIC removes interference signals partially at each stage. That is, a partial PIC adopting hard limiters cascaded to the weighting controllers of which weights are monotonically increased as the stage number increases and the interference generation is controlled by the weights. Instead of the hard limiters, soft limiters can be used and the slope of the soft limiter can be monotonically increased as the stage number increases. Also,—the soft limiter cascaded to a weighting controller can be used.

However, it is difficult to optimize the slope of the soft limiter and the weighting value at each stage. Particularly, it is more difficult to optimize the slope of the soft limiter and the weighting value at each stage when a power control is failed or the interference between time varying channels becomes stronger as the number of users increases.

Therefore, the interference canceller which can efficiently remove IPI and MAI at of the time varying channels with simple slope control method or weight control method is required.

Disclosure of Invention

It is, therefore, an object of the present invention

to provide a multistage adaptive partial parallel interference canceller (PIC) for removing multiple access interference (MAI) and interpath interference (IPI) on time varying fading channel by adaptively controlling the weights cascaded to the soft limiters.

It is another object of the present invention to provide a multistage adaptive partial PIC for minimizing the degradation of orthogonality among user signals by normalizing the output signals of the rake receiver with the estimated path gains of the rake receiver.

It is still another object of the present invention to provide a multistage adaptive partial PIC for reducing the circuit complexity by storing the output signals of the rake receiver or the matched filter in the memory and repeatedly using the value stored in the memory.

In accordance with one aspect of the present invention, there is provided a multistage adaptive partial parallel interference canceller (PIC) in a downlink receiver having a plurality of channels, for removing multiple access interference (MAI) and interpath interference (IPI), including: a filter matched to a desired walsh code and a scrambling code for despreading and integrating output signals of a rake receiver; a soft limiter for performing soft decisions and generating a soft-limited signal; a weighting control unit cascaded to the soft limiter for controlling a slope of the soft limiter; a re-spreading unit for resspreading the soft-limited signal outputted from

the soft limiter based on a walsh code and a scrambling code, and generating a re-spread signal; an interference generator for computing MAI and IPI included in the signal received at the rake receiver; and an interference signal removing unit for removing the MAI and IPI from a signal received at the rake receiver.

In accordance with another aspect of the present invention, there is provided a multistage adaptive partial parallel interference canceller (PIC) in a downlink receiver having a plurality of channels, for removing multiple access interference (MAI) and interpath interference (IPI), including: a filter matched to a desired walsh code and a scrambling code for despreading and integrating output signal of a rake receiver; a soft limiter for performing a soft decisions and generating a soft-limited signal; a weighting control unit cascaded to the soft limiter for controlling a slope of the soft limiter; a re-spread unit for resreading the soft-limited signal outputted from the soft limiter based on a walsh code and a scrambling code, and generating a re-spread signal; an interference generator for computing MAI and IPI included in the output signal of the rake receiver; and an interference signal removing unit for removing the MAI and IPI from the output signal of the rake receiver.

In accordance with still another aspect of the present invention, there is provided a multistage adaptive partial parallel interference canceller (PIC) in an uplink receiver

having a plurality of channels, for removing multiple access interference (MAI) and interpath interference (IPI), including: a filter matched to the desired walsh code and scrambling code for despreading and integrating an output
5 signal of the rake receiver; a soft limiter for performing a soft decisions and generating a soft-limited signal; a weighting control unit cascaded to the soft limiter for controlling a slope of the soft limiter; a re-spreading unit for resspreading the soft-limited signal outputted from
10 the soft limiter based on a walsh code and a scrambling code, and generating a re-spread signal; an interference generator for computing MAI and IPI included in the signal received at the output of rake receiver; and an interference signal removing unit for removing the MAI and
15 IPI from a signal received at the rake receiver.

In accordance with still another aspect of the present invention, there is provided a multistage adaptive partial parallel interference canceller (PIC) in an uplink receiver having a plurality of channels, for removing multiple
20 access interference (MAI) and interpath interference (IPI), including: a soft limiter for performing a soft decisions and generating a soft-limited signal; a weighting control unit cascaded to the soft limiter for controlling the slope of the soft limiter; a re-spreading unit for resspreading
25 the soft-limited signal outputted from the soft limiter based on a walsh code and a scrambling code, and generating a re-spread signal; an interference generator for computing

MAI and IPI included in the output signal of the matched filter; a filter matched to a desired walsh code and a scrambling code for despreading and integrating the output signals of a rake receiver; and an interference signal removing unit for removing the MAI and IPI from an output
5 signal of the filter.

Brief Description of Drawings

10 The above and other objects and features of the present invention will become apparent from the following description of the preferred embodiments given in conjunction with the accompanying drawings, in which:

Fig. 1 is a block diagram showing a conventional multistage parallel interference canceller (PIC) having
15 hard limiters;

Fig. 2 is a block diagram showing an internal structure of an i^{th} interference canceller in Fig. 1;

Fig. 3 is a block diagram showing a multistage adaptive partial parallel interference canceller (PIC) for
20 removing an interference signal at a downlink in accordance with a preferred embodiment of the present invention;

Fig. 4 is a diagram showing a simplified structure of a transmitting unit in accordance with the preferred
25 embodiment of the present invention;

Fig. 5 is a block diagram showing a detailed structure of a receiving unit in accordance with the preferred

embodiment of the present invention;

Fig. 6 is a block diagram showing a rake receiver in accordance with the preferred embodiment of the present invention;

5 Fig. 7 is a block diagram showing an i^{th} interference canceller in accordance with the present invention;

Fig. 8 is a block diagram showing a simplified i^{th} interference canceller in accordance with the present invention;

10 Fig. 9 is a block diagram showing an interference canceller having a feedback structure in accordance with the present invention;

Fig. 10 is a block diagram showing a multistage adaptive partial PIC for removing an interference signal at
15 an uplink in accordance with the preferred embodiment of the present invention;

Fig. 11 is a block diagram showing a simplified structure of a transmitting unit shown in Fig. 10 in accordance with the preferred embodiment of the present
20 invention;

Fig. 12 is a block diagram showing a detailed structure of a receiving unit in accordance with the preferred embodiment of the present invention;

Fig. 13 is a block diagram showing a rake receiver
25 shown in Fig. 12 in accordance with the preferred embodiment of the present invention;

Fig. 14 is a block diagram showing an i^{th} interference

canceller shown in Fig. 12 in accordance with the present invention;

Fig. 15 is a block diagram showing an interference canceller having a feedback structure in accordance with
5 the present invention;

Fig. 16 is a block diagram showing a multistage adaptive partial PIC in accordance with another embodiment of the present invention;

Fig. 17 is a block diagram showing an interference
10 canceller having a feedback structure in accordance with the present invention;

Fig. 18 is a graph showing performance of the conventional PIC and the existing multistage adaptive partial PICs with the multistage adaptive partial PIC of
15 the present invention;

Fig. 19A is a graph showing a performance of an existing multistage partial PIC having soft limiters cascaded to weighting units; and

Fig. 19B is a graph showing a performance of an
20 adaptive multistage partial PIC in accordance with the present invention.

Best Mode for Carrying Out the Invention

25 Other objects and aspects of the invention will become apparent from the following description of the embodiments with reference to the accompanying drawings, which is set

forth hereinafter.

A preferred embodiment of the present invention is explained in details by dividing the embodiment into a downlink and an uplink. Hereinafter, i denotes an i^{th} interference canceller and j denotes a j^{th} channel in order to describe a certain signal as X_{ij} .

<Downlink>

Fig. 3 is a block diagram showing a multistage adaptive partial parallel interference canceller (PIC) for removing an interference signal at a downlink in accordance with a preferred embodiment of the present invention.

Referring to Fig. 3, K users are using their terminals and each terminal has m_k channels having different data rates. Data of each channel to be transmitted by the a base station are encoded and interleaved by an encoder/interleaver 32, and multiplied by a Walsh code $W_k(t)$ to separate different channels.

Then, the output signals from different channels are summed and a scrambling code $S(t)$ is multiplied to the summed signal in order to identify the base station. Each signal is transmitted over multipath fading channel and a rake receiver 36 receives the signal contaminated by white Gaussian noise $n(t)$.

Received radio frequency (RF) signals may have different amplitudes or phases resulted from reflection or diffraction made by irregular terrains and obstacles. It

is called the multi-path fading. The rake receiver 36 combines the multipath signals and maximizes the signal to noise ratio.

An output signal from the rake receiver 36 is inputted to a matched filter 38 and a signal component y_{ij} for each channel is outputted from the matched filter 38. However, the signal component y_{ij} contains multiple access interference (MAI) and inter-path interference (IPI) are contained in the signal component y_{ij} and the signal component y_{ij} is time varying. The multistage adaptive partial PIC of the present invention coupled to the rake receiver 36 is to efficiently remove MAI and IPI.

Fig. 4 is a block diagram showing a simplified structure of a transmitting unit shown in Fig. 3 in accordance with the preferred embodiment of the present invention. The transmitting unit represents a part of base station which transmits a signal to a user terminal.

Referring to Fig. 4, it is assumed that each of three users uses one channel or two channels having various data rates. The user can separately transmit voice signals and video signals through two channels.

As mention with reference to Fig. 3, the signal outputted from the encoder/interleaver 32 is multiplied by the walsh code $W_j(t)$ in order to separate channels. Then, the scrambling code $S(t)$ is multiplied to the signal in order to identify the base stations and the signal is transmitted to the user terminal over multipath fading

channel. The received signal is contaminated by the white noise $n(t)$.

Fig. 5 is a block diagram showing a detailed structure of a receiving unit shown in Fig. 3. in accordance with the preferred embodiment of the present invention. The receiving unit represents a part of mobile terminal which receives a signal from a base station.

Referring to Fig. 5, the rake receiver 36 receives a signal transmitted over multipath fading channel and contaminated by white Gaussian noise. The rake receiver 36 combines the multipath signals and maximizes the signal to noise ratio with path gains obtained from the outputs of channel estimator and the signal $x_0(t)$ is a normalized signal with squared sum of estimated multipath gains

The signal $x_0(t)$ is inputted to the matched filter 38 of each channel and an output signal y_{1j} of the matched filter, for $j=1$ to 4, is generated. The signal components y_{1j} are inputted to a first interference canceller 40 and the first interference canceller 40 outputs signals to the second interference canceller 40. The signals are subsequently inputted to a next interference cancellers 40 in this manner.

The interference signals are precisely computed and removed from the received signal by the multistage PIC 40. Finally, the more reliable information bits of each user can be obtained with a deinterleaver/decoder 42.

Fig. 6 is a block diagram showing a rake receiver

shown in Fig. 5 in accordance with the preferred embodiment of the present invention.

Referring to Fig. 6, the rake receiver 36 of the user terminal receives a signal $r(t)$ transmitted from the base station. The channel estimator 64 in the rake receiver 36 outputs tap gains $a_i(t)$, $b_i(t)$ and $c_i(t)$ of each finger and estimated signal strength $A_j(t)$ of each channel.

If the time delayed signals are received through multi-path, the received signals are multiplied by the tap gains of the channel estimator 64, summed and inputted to the matched filter 38. In order to prevent orthogonality of the signals from being damaged on the time varying channel, a normalization of the output signals from the rake receiver is suggested in the present invention. That is, the output signals of the conventional rake receiver, i.e., dashed block in Fig. 6, are divided by a sum of squared tap gains.

A normalized signal x_0 of the rake receiver 36 is inputted to the matched filter 38. An operation of the matched filter is described as an equation shown in the matched filter block 38 of Fig. 6. That is, the output signal $x_0(t)$ is multiplied by the walsh code $W_{ij}(t)$ which separates user channels and the scrambling code $S_i(t)$ which identifies the base stations, and integrated for $R_j T_c$. Herein, an R_j is a spreading gain of a j^{th} channel and $1/T_c$ is a chip rate.

An output signal $y_{1j}(t)$ of the matched filter 38 is

inputted to the first interference canceller 40 and a precise interference signal is computed by the multistage interference canceller 40.

Fig. 7 is a block diagram showing an i^{th} interference canceller shown in Fig. 5 in accordance with the present invention.

The multistage adaptive parallel PIC of the present invention includes a soft limiter and a weighting controller. A slope of the soft limiter is controlled by the weighting controller.

It is preferred that a slope-controllable hyperbolic tangent function is used as a characteristic of the soft limiter and an optimization of the slope control can be simply done by updating the weighting unit cascaded to the soft limiter. The slope of the hyperbolic tangent function at each stage is adjusted to be monotonically increased from the first stage to the last stage. Performance degradation at various channels is prevented by separately controlling the slope of each soft limiter according to channel environments of users.

Referring to Fig. 7, the slope of the soft limiter is optimized by controlling a weight ω with the weighting controller 72 cascaded to the soft limiter whose characteristic is hyperbolic tangent and slope equals to be 1. The hyperbolic tangent function is expressed as:

$$\tanh(\omega U) = \frac{e^{\omega U} - e^{-\omega U}}{e^{\omega U} + e^{-\omega U}} \quad \text{Eq. 2}$$

The weighting controller 72 controls the slope of the soft limiter 74 with LMS algorithm or an average to variance ratio estimation algorithm.

5 The LMS algorithm is described as:

For $i=1$ to N and $j=1$ to 4

$$\omega_{ij}(n+1) = \omega_{ij}(n) + \eta \left(\hat{b}_j(n) - \hat{b}_{ij}(n) \right) \left(1 - \hat{b}_{ij}(n) \right) \left(1 + \hat{b}_{ij}(n) \right) + \beta \left(\omega_{ij}(n) - \omega_{ij}(n-1) \right)$$

where η and β denote learning rate and momentum factor

Eq. 3

10 The average to variance ratio estimation algorithm is expressed as:

For $i=1$ to N and $j=1$ to 4

$$\bar{A}_{ij}(n) = \left(1 - \alpha_{ij}(n) \right) \sum_{l=0}^n \alpha_{ij}^{n-l}(l) y_{ij}(l) \hat{b}_j(l)$$

$$\bar{\sigma}_{ij}^2(n) = \left(1 - \alpha_{ij}(n) \right) \sum_{l=0}^n \alpha_{ij}^{n-l}(l) \left(y_{ij}(l) - \bar{A}_{ij}(l) \hat{b}_j(l) \right)^2$$

Eq. 4

$$\alpha_{ij}(n+1) = \begin{cases} 0 & \text{for } n = -1 \\ t & \text{where } t \text{ is approximately 1 but less than 1,} \\ & \text{when } \left(\frac{\gamma \bar{A}_{ij}(n)}{\kappa \bar{\sigma}_{ij}(n)} \right)^2 = 0, \text{ and } n \geq 0 \\ 1 - \left(\frac{\gamma \bar{A}_{ij}(n)}{\kappa \bar{\sigma}_{ij}(n)} \right)^2 & \text{when } 0 < \left(\frac{\gamma \bar{A}_{ij}(n)}{\kappa \bar{\sigma}_{ij}(n)} \right)^2 < 1, \text{ and } n \geq 0 \\ 0 & \text{when } \left(\frac{\gamma \bar{A}_{ij}(n)}{\kappa \bar{\sigma}_{ij}(n)} \right)^2 \geq 1, \text{ and } n \geq 0 \end{cases}$$

where γ is a accuracy control factor of mean estimation

for controlling $\kappa \bar{\sigma}_{ij}(n)$ to be less than $\gamma \bar{A}_{ij}(n)$, and

κ is a confidential interval control factor

representing the true mean $A(n)$ is in the range of $\bar{A}_{ij}(n) - \kappa \bar{\sigma}_{ij}(n) < A(n) < \bar{A}_{ij}(n) + \kappa \bar{\sigma}_{ij}(n)$,

$$\omega_{ij}(n+1) = \frac{\bar{A}_{ij}(n)}{\bar{\sigma}_{ij}^2(n)}$$

$$\Pi\left(\frac{t}{T}\right) \equiv \begin{cases} 1 & \text{for } -\frac{1}{2} T \pi t \leq -\frac{1}{2} T \\ 0 & \text{otherwise} \end{cases}$$

If an output signal $y_{ij}(t)$ of an the $i-1^{\text{th}}$ interference canceller is inputted to the i^{th} interference canceller, a magnitude of the j^{th} channel is determined by the soft limiter 74 having a slope controlled by the weighting controller 72. That is, the magnitude of the output signal has a soft value according to the controlled slope instead of being determined as +1 or -1.

A signal outputted from the soft limiter 74 subsequently experiences a deinterleaving, a decoding and an encoding. Then, the signal is respread by the walsh code $W_{ij}(t)$ and the scrambling code $S_i(t)$. The spread
 5 signal is inputted to an interference generator 78 and an interference signal included in each channel is computed.

The interference signal computed by the interference generator 78 is expressed as:

For $i=1$ to N and $j=1$ to 4

$$10 \quad z_i(t) = \sum_{j=1}^4 z_{ij}(t)$$

$$IPI_{ai}(t) = \bar{b}_i(t-3T_c)z_i(t-3T_c) + \bar{c}_i(t-5T_c)z_i(t-5T_c)$$

$$IPI_{bi}(t) = \bar{a}_i(t+3T_c)z_i(t+3T_c) + \bar{c}_i(t-2T_c)z_i(t-2T_c)$$

$$IPI_{ci}(t) = \bar{a}_i(t+5T_c)z_i(t+5T_c) + \bar{b}_i(t+2T_c)z_i(t+2T_c)$$

Eq. 5

$$\begin{aligned}
IPS'_{ij}(t) = & \Pi \left(\frac{t - \frac{(R_j+3)T_c}{2}}{(R_j-3)T_c} \right) \bar{b}_i(t-3T_c) z_{ij}(t-3T_c) \\
& + \Pi \left(\frac{t - \frac{(R_j+5)T_c}{2}}{(R_j-5)T_c} \right) \bar{c}_i(t-5T_c) z_{ij}(t-5T_c) \\
& + \Pi \left(\frac{t - \frac{(R_j-3)T_c}{2}}{(R_j-3)T_c} \right) \bar{a}_i(t+3T_c) z_{ij}(t+3T_c) \\
& + \Pi \left(\frac{t - \frac{(R_j+2)T_c}{2}}{(R_j-2)T_c} \right) \bar{c}_i(t-2T_c) z_{ij}(t-2T_c) \\
& + \Pi \left(\frac{t - \frac{(R_j-5)T_c}{2}}{(R_j-5)T_c} \right) \bar{a}_i(t+5T_c) z_{ij}(t+5T_c) \\
& + \Pi \left(\frac{t - \frac{(R_j-2)T_c}{2}}{(R_j-2)T_c} \right) \bar{b}_i(t+2T_c) z_{ij}(t+2T_c), \\
IPS_{ij}(t) = & IPS'_{ij}(t) / B_i(t) \text{ where } B_i(t) = \bar{a}_i^2(t) + \bar{b}_i^2(t) + \bar{c}_i^2(t)
\end{aligned}$$

The computed interference signals with Eq. 5 are removed from the output signals of each finger of the rake receiver and the interference-removed signals are normalized by the tap gains of the rake receiver. Then, normalized signals $x_i(t)$ are outputted from the rake receiver.

The signals $r_i(t)$, $a_i(t)$, $b_i(t)$, $c_i(t)$ are time delayed signals of $r(t)$, $a_0(t)$, $b_0(t)$, $c_0(t)$ according to a processing delay upto the i^{th} interference canceller.

IPS_{ij} computed with Eq. 5 is summed with the normalized signals $x_i(t)$ outputted from the rake receiver to compensate over-removed signals.

As mentioned above, the interference signals are removed at the i^{th} interference canceller and the interference subtracted signals are passed to the filter matched to the desired walsh code and scrambling code. Then, the output signals of the matched filter are passed to the $i+1^{\text{th}}$ interference canceller.

Fig. 8 is a block diagram showing the i^{th} interference canceller simplified by modifying the computation used in the interference canceller of Fig. 7 in accordance with the present invention. The same reference numbers used in Fig. 7 are used in Fig. 8 because functions of the units are the same.

The modified computation method is expressed as:

For $i=1$ to N and $j=1$ to 4

15

$$z_i(t) = \sum_{j=1}^4 z_{ij}(t)$$

$$\begin{aligned} IPI_i'(t) = & \bar{a}_i(t) \left(\bar{b}_i(t-3T_c) z_i(t-3T_c) + \bar{c}_i(t-5T_c) z_i(t-5T_c) \right) + \\ & \bar{b}_i(t) \left(\bar{a}_i(t+3T_c) z_i(t+3T_c) + \bar{c}_i(t-2T_c) z_i(t-2T_c) \right) + \\ & \bar{c}_i(t) \left(\bar{a}_i(t+5T_c) z_i(t+5T_c) + \bar{b}_i(t+2T_c) z_i(t+2T_c) \right) \end{aligned} \quad \text{Eq. 6}$$

$$IPS_{ij}'(t) = \Pi \left(\frac{t - \frac{(R_j+3)T_c}{2}}{(R_j-3)T_c} \right) \bar{a}_i(t) \bar{b}_i(t-3T_c) z_{ij}(t-3T_c) +$$

$$\begin{aligned}
& \Pi \left(\frac{t - \frac{(R_j + 5)T_c}{2}}{(R_j - 5)T_c} \right) \bar{a}_i(t) \bar{c}_i(t - 5T_c) z_{ij}(t - 5T_c) + \\
& \Pi \left(\frac{t - \frac{(R_j - 3)T_c}{2}}{(R_j - 3)T_c} \right) \bar{b}_i(t) \bar{a}_i(t + 3T_c) z_{ij}(t + 3T_c) + \\
& \Pi \left(\frac{t - \frac{(R_j + 2)T_c}{2}}{(R_j - 2)T_c} \right) \bar{b}_i(t) \bar{c}_i(t - 2T_c) z_{ij}(t - 2T_c) + \\
& \Pi \left(\frac{t - \frac{(R_j - 5)T_c}{2}}{(R_j - 5)T_c} \right) \bar{c}_i(t) \bar{a}_i(t + 5T_c) z_{ij}(t + 5T_c) + \\
& \Pi \left(\frac{t - \frac{(R_j - 2)T_c}{2}}{(R_j - 2)T_c} \right) \bar{c}_i(t) \bar{b}_i(t + 2T_c) z_{ij}(t + 2T_c) \\
& IPS_{ij}(t) = IPS'_{ij}(t) / B_i(t) \quad \text{where } B_i(t) = \bar{a}_i^2(t) + \bar{b}_i^2(t) + \bar{c}_i^2(t) \\
& IPI_i(t) = IPI'_i(t) / B_i(t)
\end{aligned}$$

5 The interference signals computed by the interference generator 78 are removed at the signal x_{i0} instead of being removed at each finger. The signal x_{i0} is time shifted as much as the processing delay of the i^{th} interference canceller.

10 Fig. 9 is a block diagram showing an i^{th} interference canceller having a feedback structure in accordance with the present invention. Because a plurality of interference cancellers repeat the same function at each stage, the multistage adaptive partial PIC can be implemented in a

simple structure by storing the output signal of the rake receiver and using the stored signal repeatedly.

Referring to Fig. 9, the signal x_0 outputted from the rake receiver is stored in the first memory 85. The second
5 memory 86 stores the walsh code W_j of each channel, the scrambling code S and the magnitudes A_j of signal received at each channel.

The interference signals IPI_i computed by the interference generator 84 are removed from the signal x_0
10 outputted from the rake receiver and the interference-removed signal is stored in the third memory 87. Also, the forth memory 88 stores the tap gains a , b and c outputted from the channel estimator.

A signal processing unit 89 could be a device packaged
15 by an application specific integrated circuit (ASIC) or a digital signal processor (DSP). The signal processing unit 89 includes a matched filter, a weighting controller, a soft limiter, a deinterleaver/decoder, an encoder/interleaver and a spreader, and executes each
20 function subsequently.

An operation process of the interference canceller of Fig. 9 is the same as that of Fig. 8. That is, the interference signals IPI_i computed by the interference generator 84 are removed from the signal x_0 outputted from
25 the rake receiver and the interference-removed signal is stored in the third memory 87. The signal stored in the third memory 87 is compensated by the IPS_{ij} and inputted to

the signal processing unit 89. Herein, the IPS_{ij} computed by the Eq. 6 compensates the over-removed signal.

The signal processing unit 89 executes the functions of the matched filter, the weighting controller, the soft
5 limiter, the deinterleaver/decoder, the encoder/interleaver and the spreader, and outputs the signal to the interference generator 78. Herein, the spreader of the signal processing unit 89 re-spreads the received signal by using the Walsh code W_j of each channel, the scrambling
10 code S and the magnitudes A_j of a received signal at each channel that are stored in the second memory 36.

The interference generator 78 more precisely computes the interference signals by using the re-spread signal and the tap gains stored in the fourth memory 88. The computed
15 interference signals are removed from the signal x_0 outputted from the rake receiver 36 and the interference-removed signal is stored in the first memory 85. As the feedback is repeated, the more precise interference signals are computed. If the interference signals are converged,
20 the converged interference signals are removed from the signal outputted from the rake receiver and the desired user's signal is extracted.

Therefore, the disadvantage of the nonlinear MUD is overcome by using the feedback structure and the circuit
25 complexity can be drastically reduced.

<Uplink>

Fig. 10 is a block diagram showing a multistage adaptive partial PIC for removing an interference signal at an uplink in accordance with the preferred embodiment of the present invention.

Referring to Fig. 10, K users are using their terminals and each terminal has m_k channels having different data rates. Data of each channel to be transmitted by a mobile terminal are encoded and interleaved by an encoder/interleaver 102, and multiplied by a Walsh code $W_k(t)$.

Then, the output signals of channels are summed and a scrambling code $S_j(t)$ is multiplied to the summed signal in order to identify the mobile terminal. Each signal is transmitted over multipath fading channel and a rake receiver 106 receives the signal contaminated by white Gaussian noise $n(t)$.

An output signal from the rake receiver 106 is inputted to a matched filter 108 and a signal component y_{ij} for each channel is outputted from the matched filter 108. However, the signal component y_{ij} that contains multiple access interference (MAI) and inter-path interference (IPI) is time varying. Therefore, the multistage adaptive partial PIC of the present invention coupled to rake receiver is to efficiently remove MAI and IPI.

Fig. 11 is a block diagram showing a simplified structure of a transmitting unit shown in Fig. 10 in

accordance with the preferred embodiment of the present invention. The transmitting unit represents a part of mobile terminal which transmits a signal to a base station.

Referring to Fig. 11, it is assumed that each of three
5 users uses one channel or two channels having various data rates. The user can separately transmit voice signals and video signals through two channels.

As mentioned with reference to Fig. 10, the signal outputted from the encoder/interleaver 102 is multiplied
10 with the walsh code $W_j(t)$ in order to separate channels. Then, the scrambling code $S_j(t)$ is multiplied to the signal in order to identify the mobile terminal and the signal is transmitted to the base station over multipath fading channel. The received signal is contaminated by the white
15 noise $n(t)$.

Fig. 12 is a block diagram showing a detailed structure of a receiving unit shown in Fig. 10 in accordance with the preferred embodiment of the present invention. The receiving unit represents a part of base
20 station which receives a signal from mobile terminals.

Referring to Fig. 12, the rake receiver 106 receives a signal transmitted over multipath fading channel and contaminated by white Gaussian noise. The rake receiver 106 combines the multipath signals and maximizes the signal
25 to noise ratio with path gains obtained from the outputs of channel estimator and the signal $x_j(t)$ is a normalized signal with squared sum of estimated multipath gains. The

signal $x_j(t)$ is inputted to the matched filter 108 of each channel and its output signals y_{1j} , for $j=1\sim 4$, is generated. The signals y_{1j} are inputted to the first interference canceller 120 and output signals from the first interference canceller 120 are inputted to the second interference canceller 120. The signals are subsequently inputted to next interference cancellers in this manner.

The interference signals are precisely computed and removed from the received signal of each channel by the multistage interference canceller 120. Then, more reliable information bits of each user can be obtained with a deinterleaver/decoder 122.

Fig. 13 is a block diagram showing a rake receiver shown in Fig. 12 in accordance with the preferred embodiment of the present invention.

Referring to Fig. 13, the rake receiver 106 of the base station receives a signal $r(t)$ transmitted from the mobile terminal. The channel estimator 134 in the rake receiver 106 outputs tap gains $a_{ij}(t)$, $b_{ij}(t)$ and $c_{ij}(t)$ of each finger and estimated signal strength $A_j(t)$ of each channel

If the time delayed signals are received through multi-path, the received signals are multiplied by the tap gains of the channel estimator 134, summed and inputted to the matched filter 108. In order to prevent orthogonality of the signals from damaged on the time varying channel, a normalization of the output signals from the rake receiver

is suggested in the present invention. That is, the output signals of the conventional rake receiver, i.e., dashed block in Fig. 13, are divided by a sum of squared tap gains.

A normalized signal x_j of the rake receiver 106 is inputted to the matched filter 108. A matching operation of the matched filter x_j is described as an equation in the matched filter block 108 of Fig. 13. That is, the output signal $x_j(t)$ is multiplied by the walsh code $W_j(t)$ which separates user channels and the scrambling code $S_j(t)$ which identifies the mobile terminal, and integrated for $R_j T_c$. Herein, an R_j is a spreading gain of a j^{th} channel and $1/T_c$ is a chip rate.

An output signal $y_{1j}(t)$ of the first matched filter 108 is inputted to the first interference canceller 120 and a precise interference signal is computed by the multistage interference canceller 120.

Fig. 14 is a block diagram showing the i^{th} interference canceller shown in Fig. 12 in accordance with the present invention.

The multistage adaptive parallel PIC of the present invention includes a soft limiter and a weighting controller. A slope of the soft limiter is controlled by the weighting controller.

It is preferred that a slope-controllable hyperbolic tangent function is used as a characteristic of the soft limiter and an optimization of the slope control can be simply done by updating the weighting unit cascaded to the

soft limiter. The slope of the hyperbolic tangent function at each stage is adjusted to be monotonically increased from the first stage to the last stage. Performance degradation at various channels is prevented by separately
5 controlling the slope of each soft limiter according to channel environments of users.

Referring to Fig. 14, the slope of the soft limiter is optimized by controlling a weight w at the weighting controller 142 cascaded to the soft limiter whose
10 characteristic is hyperbolic tangent of Eq. 2 and slope equals to be 1.

The weighting controller 142 controls the slope of the soft limiter 144 with LMS algorithm or average to variance ratio estimation algorithm.

15 The LMS algorithm and the average to variance ratio estimation algorithm are the same as the ones described in the downlink.

If an output signal $y_{ij}(t)$ of an the $i-1^{\text{th}}$ interference canceller is inputted to the i^{th} interference canceller, a
20 magnitude of the j^{th} channel is determined by the soft limiter 144 having a slope controlled by the weighting controller 142. That is, the magnitude of the output signal has a soft value according to the controlled slope instead of being determined as +1 or -1.

25 A signal outputted from the soft limiter 144 subsequently experiences a deinterleaving, a decoding and an encoding. Then, the signal is respread by the walsh

code $W_{ij}(t)$ and the scrambling code $S_{ij}(t)$. The spread signal is inputted to an interference generator 148 and an interference signal included in each channel is computed.

The interference signal computed by the interference generator 148 is expressed as:

$$\begin{aligned}
 & \text{For } j=1 \text{ to } 4 \text{ and } i=1 \text{ to } N \\
 & z_{oij}(t) = (\bar{a}_{ij}(t)z_{ij}(t) + \bar{b}_{ij}(t-3T_c)z_{ij}(t-3T_c) + \bar{c}_{ij}(t-5T_c)z_{ij}(t-5T_c)) \\
 & MAI_{oij}(t) = \sum_{\substack{l=1 \\ l \neq j}}^4 z_{oil}(t) \\
 & MAI_{ij}(t) = (\bar{a}_{ij}(t)MAI_{oij}(t) + \bar{b}_{ij}(t)MAI_{oij}(t+3T_c) + \bar{c}_{ij}(t)MAI_{oij}(t+5T_c)) \\
 & IPI_{ij}(t) = \Pi\left(\frac{t-\frac{3}{2}T_c}{3T_c}\right)\bar{a}_{ij}(t)\bar{b}_{ij}(t-3T_c)z_{ij}(t-3T_c) + \Pi\left(\frac{t-\frac{5}{2}T_c}{5T_c}\right)\bar{a}_{ij}(t)\bar{c}_{ij}(t-5T_c)z_{ij}(t-5T_c) \\
 & \quad + \Pi\left(\frac{t-(R_j-\frac{3}{2})T_c}{3T_c}\right)\bar{b}_{ij}(t)\bar{a}_{ij}(t+3T_c)z_{ij}(t+3T_c) + \Pi\left(\frac{t-T_c}{2T_c}\right)\bar{b}_{ij}(t)\bar{c}_{ij}(t-2T_c)z_{ij}(t-2T_c) \\
 & \quad + \Pi\left(\frac{t-(R_j-\frac{5}{2})T_c}{5T_c}\right)\bar{c}_{ij}(t)\bar{a}_{ij}(t+5T_c)z_{ij}(t+5T_c) + \Pi\left(\frac{t-(R_j-1)T_c}{2T_c}\right)\bar{c}_{ij}(t)\bar{b}_{ij}(t+2T_c)z_{ij}(t+2T_c) \\
 & I_{ij}(t) = (MAI_{ij}(t) + IPI_{ij}(t)) / B_{ij}(t), \quad \text{where } B_{ij}(t) = \bar{a}_{ij}^2(t) + \bar{b}_{ij}^2(t) + \bar{c}_{ij}^2(t)
 \end{aligned}$$

Eq. 7

The computed interference signals with Eq. 7 are removed from the normalized output signals x_{ij} of the rake receiver.

The signals $r_{ij}(t)$, $a_{ij}(t)$, $b_{ij}(t)$, $c_{ij}(t)$ are time delayed signals of $r(t)$, $a_{0j}(t)$, $b_{0j}(t)$, $c_{0j}(t)$ according to a processing delay upto the i^{th} interference canceller.

As mentioned above, the interference signals are

removed at the i^{th} interference canceller and the interference subtracted signals are passed to the filter matched to the desired walsh code and scrambling code. Then, the output signals of the matched filter are passed
5 to the $i+1^{\text{th}}$ interference canceller.

Fig. 15 is a block diagram showing the interference canceller having a feedback structure in accordance with the present invention. Because a plurality of interference cancellers repeat the same function at each stage, the
10 multistage adaptive partial PIC can be implemented in a simple structure by storing the output signals of the rake receiver and using the stored signals repeatedly.

Referring to Fig. 15, the signal x_j outputted from the rake receiver 106 is stored in the first memory 135. The
15 second memory 136 stores the Walsh code W_j of each channel, the scrambling code S_j and the magnitudes A_j of signal received at each channel.

The interference signals I_{ij} computed by the interference generator 148 are removed from the signal x_j
20 outputted from the rake receiver and the interference-removed signal is stored in the third memory 137. Also, the fourth memory 138 stores the tap gains a , b and c outputted from the channel estimator.

A signal processing unit 139 could be a device
25 packaged by the application specific integrated circuit (ASIC) or the digital signal processor (DSP). The signal processing unit 139 includes a matched filter, a weighting

controller, a soft limiter, a deinterleaver/decoder, a encoder/interleaver and a spreader, and executes each function subsequently.

An operation process of the interference canceller of Fig. 15 is the same as that of Fig.14. That is, the interference signals I_{ij} computed by the interference generator 148 are removed from the signal x_j outputted from the rake receiver and the interference-removed signal is stored in the third memory 137. The signal stored in the third memory 137 is inputted to the signal processing unit 139.

The signal processing unit 139 executes the functions of the matched filter, the weighting controller, the soft limiter, the deinterleaver/decoder, the encoder/interleaver and the spreader, outputs the signal to the interference generator 148. Herein, the spreader of the signal processing unit 139 re-spreads the received signal by using the walsh code W_j of each channel, the scrambling code S_j and the magnitudes A_j of a received signal at each channel stored in the second memory 136.

The interference generator 148 more precisely computes the interference signals by using the re-spread signal and the tap gains stored in the fourth memory 138. The computed interference signals are removed from the signal x_j outputted from the rake receiver 106 and stored in the first memory 135. As the feedback is repeated, the more precise interference signals are computed. If the

interference signals are converged, the converged interference signals are removed from the signal outputted from the rake receiver and the desired user's information bits are extracted.

5 Therefore, the disadvantage of the nonlinear MUD is overcome by using the feedback structure and the circuit complexity can be drastically reduced.

Fig. 16 is a block diagram showing a multistage adaptive partial PIC in accordance with another embodiment
10 of the present invention.

Although an operation process of the multistage adaptive partial PIC of Fig. 16 is similar to that of Fig. 14, computation process of interference signal is modified and the interference signal is removed at the output port
15 of the matched filter 108. The circuit is more simplified by removing the interference signal at the output port of the matched filter.

The modified equation for computing the interference signals is expressed as:

20

For $j=1$ to 4 and $i=1$ to N

$$z_{oij}(t) = (\bar{a}_{ij}(t)z_{ij}(t) + \bar{b}_{ij}(t-3T_c)z_{ij}(t-3T_c) + \bar{c}_{ij}(t-5T_c)z_{ij}(t-5T_c))$$

$$MAI_{oij}(t) = \sum_{\substack{l=1 \\ l \neq j}}^4 z_{oil}(t)$$

Eq. .8

$$\begin{aligned}
MAI_{ij}(t) &= (\bar{a}_{ij}(t)MAI_{\alpha ij}(t) + \bar{b}_{ij}(t)MAI_{\alpha ij}(t+3T_c) + \bar{c}_{ij}(t)MAI_{\alpha ij}(t+5T_c)) \\
IPI_{ij}(t) &= \Pi\left(\frac{t-\frac{3}{2}T_c}{3T_c}\right)\bar{a}_{ij}(t)\bar{b}_{ij}(t-3T_c)z_{ij}(t-3T_c) + \Pi\left(\frac{t-\frac{5}{2}T_c}{5T_c}\right)\bar{a}_{ij}(t)\bar{c}_{ij}(t-5T_c)z_{ij}(t-5T_c) \\
&+ \Pi\left(\frac{t-(R_j-\frac{3}{2})T_c}{3T_c}\right)\bar{b}_{ij}(t)\bar{a}_{ij}(t+3T_c)z_{ij}(t+3T_c) + \Pi\left(\frac{t-T_c}{2T_c}\right)\bar{b}_{ij}(t)\bar{c}_{ij}(t-2T_c)z_{ij}(t-2T_c) \\
&+ \Pi\left(\frac{t-(R_j-\frac{5}{2})T_c}{5T_c}\right)\bar{c}_{ij}(t)\bar{a}_{ij}(t+5T_c)z_{ij}(t+5T_c) + \Pi\left(\frac{t-(R_j-1)T_c}{2T_c}\right)\bar{c}_{ij}(t)\bar{b}_{ij}(t+2T_c)z_{ij}(t+2T_c) \\
I_{ij}(t) &= (MAI_{ij}(t) + IPI_{ij}(t)) / B_{ij}(t), \quad \text{where } B_{ij}(t) = \bar{a}_{ij}^2(t) + \bar{b}_{ij}^2(t) + \bar{c}_{ij}^2(t) \\
\bar{I}_{ij}(t) &= \frac{1}{R_j T_c} \int_0^{R_j T_c} I_{ij}(t) W_{ij}(t) S_{ij}(t) dt
\end{aligned}$$

5 The output signal x_{ij} is inputted to the matched filter 108 and the signal \bar{x}_{ij} is outputted. The interference signal \bar{I}_{ij} computed in the interference generator 148 is removed from the signal \bar{x}_{ij} .

10 Fig. 17 is a block diagram showing the i^{th} interference canceller having a feedback structure in accordance with the present invention. The same reference numbers of Fig. 15 are used in Fig. 17 because the functions of the units are the same.

15 Referring to Fig. 17, the signal x_j outputted from the rake receiver 106 is inputted to the matched filter 108 and the matched filter output signal \bar{x}_j is stored in the first memory 135.

 The interference signal \bar{I}_{ij} computed by the interference generator 148 is removed from the matched

filter output signal \bar{x}_j stored in the first memory 135 and the interference-removed signal is stored in the third memory 137. The interference-removed signal stored in the third memory 137 is inputted to the signal processing unit
5 139.

The signal processing unit 139 includes the matched filter, a weighting controller, a soft limiter, a deinterleaver/decoder, an encoder/interleaver, and a spreader, and executes each function subsequently. Herein,
10 the spreader of the signal processing unit 139 re-spreads the received signal by using the Walsh code W_j of each channel, the scrambling code S_j and the magnitudes A_j of a received signal at each channel stored in the second memory 136.

15 The interference generator 148 more precisely computes the interference signals by using the re-spread signal and the tap gains stored in the fourth memory 138. The computed interference signal is removed from the signal \bar{x}_j outputted from the matched filter 108 and stored in the first memory 135. As the feedback is repeated, the more precise interference signals are computed. If the interference signals are converged, the converged interference signals are removed from the signal outputted from the rake receiver and the desired user's information
20 bits are extracted.
25

<Simulation Results>

The performance of the invented multistage adaptive partial PIC are evaluated for the uplink channels which are assumed to have the system parameters summarized in Table 1.

5 [Table 1]

Items	Parameters
Number of users	3 - 4
Multiple-access mode	DS-CDMA
Chip rate	3.84 Mcps
Modulation	BPSK
Spreading code	Short Scrambling Code(Length : 256)
	Walsh code
Spreading gain	4
Channel coding	Turbo Code , Coding Rate 1/3,
Channel model	COST207. model for urban area 3 - path channel assumed (path delay : $0T_c$, $1 T_c$, $2 T_c$)

The performance of the conventional PIC, the existing multistage partial PICs, and the multistage adaptive partial PIC of the present invention are compared in Fig.
10 18.

The reference number 181 represents a performance of the conventional multistage PIC and the reference number 182 illustrates a performance of the five-stage partial PIC
15 which consists of fixed slope soft limiters followed by the weighting units. The weight values of each stage are chosen as the ones that show the best BER performance at the last stage by test. The reference number 183 shows a performance of the five-stage partial PIC which includes
20 only soft limiters. The slopes of each stage are chosen as

the ones that show the best BER performance by test. The reference number 184 shows a performance of a two-stage adaptive partial PIC of the present invention.

Referring to Fig. 18, the two-stage adaptive partial
5 PIC of the present invention outperforms the conventional multistage PIC and existing five-stage partial PICs. When bit error rate (BER) is assumed as 10^{-3} , an obtained gain is 2-3 dB and the performance of the present invention is almost same as an optimal performance 185 of single user
10 channel which has no MAI.

Fig. 19A shows a performance of a multistage partial PIC controlling weighting values at each stage and slopes of soft limiters; and Fig. 19B depicts a performance of an adaptive multistage partial PIC of the present invention.

Referring to Figs. 19A and 19B, the performance of the
15 multistage partial PIC can be enhanced and the error floor problem can be solved more efficiently by adaptively controlling the only slopes of the soft limiters than multistage partial PIC which controls the slopes of the
20 soft limiters and the weighting values together.

As mentioned above, with the present invention MAI and IPI on the time varying fading channel can be removed by adaptively controlling the slope of the soft limiter with the weighting controller cascaded to the soft limiter.

Also, the degradation of orthogonality among user
25 signals is minimized by normalizing the output signals of the rake receiver with the sum of squared path gains

obtained from the channel estimator.

Also, the circuit complexity can be reduced by storing the output signals of the rake receiver or the matched filter in the memory and canceling the estimated
5 interference from the stored values with the feedback structured recursive adaptive partial PIC.

While the present invention has been shown and described with respect to the particular embodiments, it will be apparent to those skilled in the art that many
10 changes and modifications may be made without departing from the spirit and scope of the invention as defined in the appended claims.